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## IN THE CLAIMS:

The following is a listing of all the claims as they currently stand. Kindly cancel claims 43-53 and 99-111, amend claims 1-42 and 54-98, and add claims 112-123, as noted below.

- 1. (Currently amended) A system for analyzing the use of medical devices comprising:
- a) a geometry generator that receives three-dimensional volumetric data of at least one anatomical feature and generates a geometric model of said anatomical feature(s);
- b) a mesh generator that receives the said geometric model of said anatomical feature(s) and the a geometric model of a medical device, and generates a finite element model or mesh incorporating based on both of said geometric model of said anatomical feature(s) and said geometric model of said medical device; and
- e) a stress/strain/deformation analyzer that receives said finite element model or mesh incorporating both said anatomical feature and said medical device, material[[s]] properties of said anatomical feature(s) and said medical device, and load data on said anatomical feature(s) and/or said medical device[[,]] and simulates an interaction between said anatomical feature(s) and said medical device to determine the predicted stresses, strains, and deformations of, said medical device.
- 2. (Currently amended) A <u>The</u> system as defined in of claim 1 where in said geometric model of said anatomical feature(s) is an idealized geometric model.
- 3. (Currently amended) A <u>The</u> system as defined in of claim 1 wherein said three-dimensional volumetric data are acquired via CT scan.

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- 4. (Currently amended) A <u>The</u> system as defined in of claim 1 wherein said three-dimensional volumetric data are acquired via MRI.
- 5. (Currently amended) A <u>The</u> system as defined in of claim 1 where <u>in</u> said geometric model of a said medical device is for an endovascular prosthesis.
- 6. (Currently amended) A <u>The</u> system as defined in of claim 5 wherein said endovascular prosthesis is a transluminally placed endovascular graft.
- 7. (Currently amended) A <u>The</u> system as defined in of claim 5 wherein said endovascular prosthesis is a cardiovascular stent device.
- 8. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 1 where<u>in</u> said geometry generator is MIMICS.
- 9. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 1 where<u>in</u> said mesh generator is TRUEGRID.
- 10. (Currently amended) A <u>The</u> system as defined in of claim 1 wherein said stress/strain/deformation analyzer is DYNA3D.
- 11. (Currently amended) A <u>The</u> system as defined in of claim 1 wherein said stress/strain/deformation analyzer is NIKE3D.
- 12. (Currently amended) A <u>The</u> system-as defined in of claim 10 wherein said DYNA3D is modified to accommodate a strain energy density of the form:

W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 +$$

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$$a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + \frac{1}{2}K(I_3-1)^2$$

with 
$$K = 2(a_{10} + a_{01}) / (1 - 2\nu)$$

where

a;; are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and  $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

13. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 11 where<u>in</u> said NIKE3D is modified to accommodate a strain energy density of the form:

W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 + a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + a_{12}(I_3-1)^2$$

with 
$$K = 2(a_{10} + a_{01}) / (1 - 2\nu)$$

where

 $a_{ij}$  are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and  $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

14. (Currently amended) A <u>The</u> system as defined in of claim 1 further comprising a visualization tool that receives said <u>simulated</u> stresses, and strains, and

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deformations of on said medical device and anatomical feature from said stress/strain/deformation analyzer and displays one or more of said stresses, and strains, and deformations of on said medical device via visual representation.

- 15. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 14 where<u>in</u> said visualization tool is GRIZ.
- 16. (Currently amended) A system for analyzing the use of a medical device comprising:
- a) a geometry generator that receives three-dimensional volumetric data of at least one anatomical feature of a particular individual and generates a geometric model of said anatomical feature(s);
- b) a mesh generator that receives the said geometric model of said anatomical feature(s) and the a geometric model of a medical device, and generates a finite element model or mesh incorporating based on both said geometric model of said anatomical feature(s) and said geometric model of said medical device; and
- e) a stress/strain/deformation analyzer that receives said finite element model or mesh incorporating both said anatomical feature and said medical device, material[[s]] properties of said anatomical feature(s) and said medical device, and load data on said anatomical feature(s) and/or said medical device[[,]] and simulates an interaction between said anatomical feature(s) and said medical device to determine the predicted stresses, strains, and deformation of, said medical device.
- 17. (Currently amended) A <u>The</u> system as <u>defined in of claim 16</u> where<u>in</u> said geometric model of said anatomical feature(s) is an idealized geometric model.

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18. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 16 where<u>in</u> said three-dimensional volumetric data are acquired via CT scan.

- 19. (Currently amended) A <u>The</u> system-as defined in of claim 16 wherein said three-dimensional volumetric data are acquired via MRI.
- 20. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 16 where<u>in</u> said geometric model of a said medical device is for an endovascular prosthesis.
- 21. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 20 where<u>in</u> said endovascular prosthesis is a transluminally placed endovascular stent graft.
- 22. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 20 where<u>in</u> said endovascular prosthesis is a cardiovascular stent device.
- 23. (Currently amended) A <u>The</u> system as defined in of claim 16 where in said geometry generator is MIMICS.
- 24. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 16 where<u>in</u> said mesh generator is TRUEGRID.
- 25. (Currently amended) A <u>The</u> system as defined in of claim 16 where in said stress/strain/deformation analyzer is DYNA3D.
- 26. (Currently amended) A <u>The</u> system as defined in of claim 16 wherein said stress/strain/deformation analyzer is NIKE3D.

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27. (Currently amended) A <u>The</u> system as defined in of claim 25 wherein said DYNA3D is modified to accommodate a strain energy density of the form:

W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 + a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + a_{12}K(I_3-1)^2$$

with 
$$K = 2(a_{10} + a_{01}) / (1 - 2v)$$

where

a;; are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and  $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

28. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 26 where<u>in</u> said NIKE3D is modified to accommodate a strain energy density of the form:

W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 + a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + a_{12}K(I_3-1)^2$$

with 
$$K = 2(a_{10} + a_{01}) / (1 - 2v)$$

where

a<sub>ij</sub> are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and  $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

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- 29. (Currently amended) A <u>The</u> system as defined in of claim 16 further comprising a visualization tool that receives said <u>simulated</u> stresses, and strains, and <u>deformations of</u>, on said medical device and anatomical feature from said <u>stress/strain/deformation analyzer</u> and displays <u>one or more of</u> said stresses, and strains, and <u>deformations on of</u>, said medical device via visual representation.
- 30. (Currently amended) A <u>The</u> system as defined in of claim 29 wherein said visualization tool is GRIZ.
- 31. (Currently amended) A system for analyzing the use of <u>a</u> medical device comprising:
- a) a mesh generator that receives a geometric model of an in vitro anatomical feature and a geometric model of a medical device, and generates a finite element model or mesh incorporating based on both said geometric model of said in vitro anatomical feature and said geometric model of said medical device; and
- b) <u>a</u> stress/strain/deformation analyzer that receives said <u>finite element model or</u> mesh incorporating both said anatomical feature and said medical device, material[[s]] properties of said <u>in vitro</u> anatomical feature and said medical device, and load <u>data</u> on said <u>in vitro</u> anatomical feature and/or said medical device[[,]] and simulates an interaction between said <u>in vitro</u> anatomical feature and said medical device to determine the predicted stresses, strains, and deformations on <u>of</u>, said medical device.
- 32. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 31 where <u>in</u> said in vitro <u>anatomical</u> feature is a geometric model of an idealized <u>anatomical</u> feature.
- 33. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 31 where<u>in</u> said geometric model of said medical device is for an endovascular prosthesis.

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- 34. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 33 where<u>in</u> said endovascular prosthesis is a <u>transluminally placed endovascular</u> <u>stent</u> graft.
- 35. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 33 where<u>in</u> said endovascular prosthesis is a cardiovascular stent device.
- 36. (Currently amended) A <u>The</u> system as defined in of claim 31 wherein said mesh generator is TRUEGRID.
- 37. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 31 where<u>in</u> said stress/strain/deformation analyzer is DYNA3D.
- 38. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 31 where<u>in</u> said stress/strain/deformation analyzer is NIKE3D.
- 39. (Currently amended) A <u>The</u> system as defined in <u>of</u> claim 37 where<u>in</u> said DYNA3D is modified to accommodate a strain energy density of the form:

W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 + a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + a_{12}(I_3-1)^2$$

with 
$$K = 2(a_{10} + a_{01}) / (1 - 2\nu)$$

where

a;; are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and

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 $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

40. (Currently amended) A <u>The</u> system as defined in of claim 38 wherein said NIKE3D is modified to accommodate a strain energy density of the form:

W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 + a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + a_{12}(I_3-1)^2$$

with 
$$K = 2(a_{10} + a_{01}) / (1 - 2v)$$

where

a;; are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and  $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

- 41. (Currently amended) A <u>The</u> system as <u>defined in of claim 31</u> further comprising <u>a visualization tool that receives said <u>simulated</u> stresses, <u>and strains, and deformations of</u>, on said medical device <u>and anatomical feature from said stresses</u>, and strains, and deformations of, on said medical device via visual representation.</u>
- 42. (Currently amended) A <u>The</u> system as defined in of claim 41 wherein said visualization tool is GRIZ.

43. to 53. (Canceled)

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- 54. (Currently amended) A computer method for analyzing a medical device comprising:
  - a) acquiring three-dimensional volumetric data of at least one anatomical feature;
- b) generating a geometric model of said three-dimensional volumetric data anatomical feature(s);
- e) receiving data representing a geometric model of a candidate medical device design;
- d) receiving said geometric model of said three-dimensional volumetric data anatomical feature(s);
- e) generating a <u>finite element model or</u> mesh <u>incorporating based on</u> both said geometric model of said anatomical feature and said geometric model of said candidate medical device design;
- f) receiving material properties of said mesh anatomical feature(s) and said candidate medical device design;
- g) receiving load data imposed on of said mesh candidate medical device design and said anatomical feature(s); and
- h) simulating an interaction between said anatomical feature(s) and said candidate medical device design to determine the predicted stresses, strains, and deformation of imposed on said candidate medical device design by said load data.
- 55. (Currently amended) A <u>The</u> method as defined in of claim 54 further emprising wherein the step of simulating stresses, strains, and deformations is performed to a point of failure of said candidate medical device design.
- 56. (Currently amended) A <u>The</u> method as defined in of claim 54 wherein said three-dimensional volumetric data are acquired via CT scan.

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- 57. (Currently amended) A <u>The</u> method as defined in of claim 54 wherein said three-dimensional volumetric data are acquired via MRI.
- 58. (Currently amended) A <u>The</u> method as <u>defined in of claim 54</u> where<u>in said geometric model of a candidate medical device <u>design</u> is for an endovascular prosthesis.</u>
- 59. (Currently amended) A <u>The</u> method as defined in of claim 58 where <u>in</u> said endovascular prosthesis is a transluminally placed endovascular stent graft.
- 60. (Currently amended) A <u>The</u> method as defined in of claim 58 wherein said endovascaular endovascular prosthesis is a cardiovascular stent device.
- 61. (Currently amended) A <u>The</u> method as defined in of claim 54 wherein said geometric model for three-dimensional volumetric data said anatomical feature(s) is generated by a MIMICS software application.
- 62. (Currently amended) A The method as defined in of claim 54 wherein said step of generating a finite element model or mesh is generated performed by using TRUEGRID.
- 63. (Currently amended) A <u>The</u> method as defined in of claim 54 wherein said stresses, strains, and deformations are simulated by a DYNA3D software application.
- 64. (Currently amended) A <u>The</u> method as defined in of claim 54 wherein said stresses, strains, and deformations are simulated by a NIKE3D software application.

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65. (Currently amended) A <u>The</u> method as defined in of claim 63 where in said DYNA3D is modified to accommodate a strain energy density of the form:

W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 + a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + a_{12}(I_3-1)^2$$

with 
$$K = 2(a_{10} + a_{01}) / (1 - 2v)$$

where

a;; are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and  $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

66. (Currently amended) A <u>The</u> method as defined in of claim 64 where in said NIKE3D is modified to accommodate a strain energy density of the form:

W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 + a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + a_{12}K(I_3-1)^2$$

with  $K = 2(a_{10} + a_{01}) / (1 - 2\nu)$ 

where

 $a_{ij}$  are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and  $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

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- 67. (Currently amended) A <u>The</u> method as defined in of claim 54 where in said stress/strain/deformation analysis is done performed using a non-linear finite element analysis tool.
- 68. (Currently amended) A <u>The</u> method as defined in of claim 54 further comprising the step of receiving results of said stress, strain, and deformation analysis into a visualization tool and where <u>in</u> said visualization tool visually presents the <u>one</u> or <u>more of said</u> strains, stresses, and deformations on <u>of</u>, said medical device.
- 69. (Currently amended) A <u>The</u> method as defined in of claim 68 wherein said visualization means tool is GRIZ.
- 70. (Currently amended) A method for analyzing a medical device comprising:
- a) acquiring three-dimensional volumetric data of at least one anatomical feature of a particular individual;
- b) generating a geometric model of said three-dimensional volumetric data anatomical feature(s);
  - c) receiving a geometric model of a candidate medical device;
- d) receiving said geometric model of said three dimensional volumetric data anatomical feature(s);
- e) generating a mesh incorporating <u>based on</u> both said geometric model of said anatomical feature and geometric model of said candidate medical device;
- f) receiving material properties of said mesh anatomical feature(s) and said candidate medical device;
- g) receiving load <u>data-imposed on-of</u> said mesh <u>anatomical feature(s) and said</u> <u>candidate medical device</u>; and

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h) simulating an interaction between said anatomical feature(s) and said candidate medical device to determine the predicted dynamic or quasi-static stresses, strains, and deformations of imposed on said candidate medical device.

- 71. (Currently amended) A <u>The</u> method as defined in <u>of</u> claim 70 further emprising wherein the step of simulating stresses, strains, and deformations is <u>performed</u> to point of failure of said <u>candidate</u> medical device.
- 72. (Currently amended) A <u>The</u> method as defined in of claim 70 wherein said three-dimensional volumetric data are acquired via CT scan.
- 73. (Currently amended) A <u>The</u> method as defined in of claim 70 wherein said three-dimensional volumetric data are acquired via MRI.
- 74. (Currently amended) A <u>The</u> method as defined in of claim 70 wherein said geometric model of a candidate medical device is for an endovascular prosthesis.
- 75. (Currently amended) A <u>The</u> method as defined in of claim 74 wherein said endovascular prosthesis is a transluminally placed endovascular graft.
- 76. (Currently amended) A <u>The</u> method as defined in of claim 74 where <u>in</u> said endovascular prosthesis is a cardiovascular stent device.
- 77. (Currently amended) A The method as defined in of claim 70 wherein said step of generating the geometric model of said anatomical feature(s) means for three-dimensional volumetric data is performed by using MIMICS.

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- 78. (Currently amended) A <u>The</u> method as defined in claim 70 where<u>in</u> said step of mesh generating means is said mesh is performed by using TRUEGRID.
- 79. (Currently amended) A <u>The method as defined in of claim 70 where in said step of simulating dynamic or quasi-static stresses/strains/deformations simulating means is performed by using DYNA3D.</u>
- 80. (Currently amended) A <u>The method as defined in of claim 70 wherein</u> said <u>step of simulating stresses/strains/deformations simulating means</u> is <u>performed by using NIKE3D.</u>
- 81. (Currently amended) A <u>The</u> method as defined in of claim 79 wherein said DYNA3D is modified to accommodate a strain energy density of the form:

W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 + a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + a_{12}(I_3-1)^2$$

with 
$$K = 2(a_{10} + a_{01}) / (1 - 2\nu)$$

where

a;; are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and  $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

82. (Currently amended) A <u>The method as defined in of claim 80 wherein</u> said NIKE3D is modified to accommodate a strain energy density of the form:

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W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 + a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + \frac{1}{2}K(I_3-1)^2$$
  
with  $K = 2(a_{10} + a_{01}) / (1-2\nu)$ 

where

a;; are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and  $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

- 83. (Currently amended) A <u>The</u> method as defined in of claim 70 where in said stress/strain/deformation analysis is done performed using a non-linear finite element analysis tool.
- 84. (Currently amended) A <u>The</u> method as defined in of claim 70 further comprising the step of receiving results of said stress, and strain and deformation analysis into a visualization tool and where <u>in</u> said visualization tool visually presents the <u>one or more of said</u> strains, and stresses and deformations of on said medical device.
- 85. (Currently amended) A <u>The</u> method as defined in of claim 84 wherein said visualization means tool is GRIZ.
- 86. (Currently amended) A computer method for analyzing a medical device comprising:

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a) receiving data representing an a geometric model of at least one in vitro model anatomical feature and a geometric model of a candidate medical device design;

- e) generating a <u>finite element model or mesh incorporating based on</u> both said geometric model of said in vitro <u>model anatomical feature(s)</u> and <u>said</u> geometric model of said candidate medical device design;
- f) receiving material properties of said mesh in vitro anatomical feature(s) and said candidate medical device design;
- g) receiving load data <u>imposed on</u> of said <u>mesh</u> <u>in vitro</u> anatomical feature(s) and said candidate <u>medical device design</u>; and
- h) simulating an interaction between said in vitro anatomical feature(s) and said candidate medical device design to determine the predicted stresses, strains, and deformations of imposed on said candidate medical device design by said load data.
- 87. (Currently amended) A <u>The</u> method as <u>defined in of claim 86 further</u> emprising <u>wherein</u> the step of simulating stresses, and strains <u>and deformations is performed</u> to a point of failure of said <u>candidate</u> medical device <u>design</u>.
- 88. (Currently amended) A <u>The</u> method as <u>defined in of claim 86 where in said geometric model of a said candidate medical device <u>design</u> is for an endovascular prosthesis.</u>
- 89. (Currently amended) A <u>The</u> method as defined in of claim 88 wherein said endovascular prosthesis is a transluminally placed endovascular graft.
- 90. (Currently amended) A <u>The</u> method as defined in <u>of</u> claim 88 where<u>in</u> said endovascular prosthesis is a cardiovascular stent device.

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- 91. (Currently amended) A <u>The</u> method as defined in of claim 86 where in said mesh generating means is step of generating said mesh is performed by using TRUEGRID.
- 92. (Currently amended) A <u>The</u> method as defined in of claim 86 where <u>in</u> said stress/strain/deformation simulating means is step of simulating stresses, strains, and deformations is performed by using DYNA3D.
- 93. (Currently amended) A <u>The</u> method as defined in of claim 86 wherein said stress/strain/deformation simulating means is step of simulating stresses, strains, and deformations is performed by using NIKE3D.
- 94. (Currently amended) A <u>The</u> method as defined in of claim 92 wherein said DYNA3D is modified to accommodate a strain energy density of the form:

W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 + a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + \frac{1}{2}K(I_3-1)^2$$

with 
$$K = 2(a_{10} + a_{01}) / (1 - 2v)$$

where

a;; are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and  $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

95. (Currently amended) A <u>The</u> method as defined in claim 93 where<u>in</u> said NIKE3D is modified to accommodate a strain energy density of the form:

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W = 
$$a_{10}(I_1-3) + a_{01}(I_2-3) + a_{20}(I_1-3)^2 + a_{11}(I_1-3)(I_2-3) + a_{02}(I_2-3)^2 + a_{30}(I_1-3) + a_{21}(I_1-3)^2(I_2-3) + a_{12}(I_1-3)(I_2-3)^2 + a_{03}(I_2-3)^3 + a_{02}(I_3-1)^2$$

with  $K = 2(a_{10} + a_{01}) / (1 - 2\nu)$ 

where

a;; are material parameters;

v is Poisson's ratio;

K is the bulk modulus given as a function of Poisson's ratio; and  $I_1$ ,  $I_2$ , and  $I_3$  are the first, second, and third invariants of the right Cauchy-Green strain tensor, respectively.

- 96. (Currently amended) A <u>The</u> method as <u>defined in of</u> claim 86 where<u>in</u> said stress/strain/deformation analysis is <u>done performed</u> using a non-linear finite element analysis tool.
- 97. (Currently amended) A The method as defined in of claim 86 further comprising the step of receiving results of said stress, strain, and deformation analysis into a visualization tool and wherein said visualization tool visually presents the one or more of said strains, and stresses and deformations of on said candidate medical device design.
- 98. (Currently amended) A <u>The</u> method as defined in of claim 97 wherein said visualization means tool is GRIZ.

99-111. (Canceled)

Please add claims 112-123 as follows:

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(New) The system of claim 1 wherein said stress/strain/deformation 112. analyzer uses a non-linear finite element analysis tool to simulate said stresses, strains, and deformations of said medical device.

- (New) The system of claim 1 wherein said simulated stresses, strains, and 113. deformations imposed on said medical device comprise dynamic or quasi-static stresses, strains, and deformations.
- (New) The system of claim 16 wherein said stress/strain/deformation 114. analyzer uses a non-linear finite element analysis tool to simulate stresses, strains, and deformations of said medical device.
- (New) The system of claim 16 wherein said simulated stresses, strains, 115. and deformations imposed on said medical device comprise dynamic or quasi-static stresses, strains, and deformations.
- 116. (New) The system of claim 31 wherein said stress/strain/deformation analyzer uses a non-linear finite element analysis tool to simulate stresses, strains, and deformations of said medical device.
- (New) The system of claim 31 wherein said simulated stresses, strains, 117. and deformations imposed on said medical device comprise dynamic or quasi-static stresses, strains, and deformations.

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(New) The method of claim 54 wherein said simulated stresses, strains, 118. and deformations imposed on said medical device design comprise dynamic or quasi-static stresses, strains, and deformations.

- (New) The method of claim 86 wherein said simulated stresses, strains, 119. and deformations imposed on said candidate medical device design comprise dynamic or quasistatic stresses, strains, and deformations.
- 120. (New) The method of claim 86 further comprising receiving data representing a geometric model of an in vitro failure mode test.
- (New) The method of claim 120 wherein said step of simulating 121. comprises simulating stresses, strains, and deformations imposed on said candidate medical device design by said load data in said in vitro failure mode test.
- (New) The method of claim 120 further comprising varying one or more 122. in vitro failure mode test parameters based on an additional step of comparing:

simulation data generated by said step of simulating stresses, strains, and deformations imposed on said candidate medical device design by said load data representing said anatomical feature; and

additional simulation data generated by said step of simulating stresses, strains, and deformations imposed on said candidate medical device design by said load data in said in vitro failure mode test.

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123. (New) The method of claim 122 wherein said one or more *in vitro* failure mode test parameters further comprises test frequency.